

**PATENT****IN THE UNITED STATES PATENT AND TRADEMARK OFFICE**

Appl. No.: 10/263,135 Confirmation No.: 2687  
Applicant(s): Fritzemeier et al.  
Filed: October 2, 2002  
Art Unit: 1742  
Examiner: Jenkins, Daniel J.  
Title: METHOD FOR PREPARING CRYOMILLED ALUMINUM ALLOYS  
AND COMPONENTS EXTRUDED AND FORGED THEREFROM

Docket No.: 038190/234776  
Customer No.: 00826

October 27, 2004

Commissioner for Patents  
P.O. Box 1450  
Alexandria, Virginia 22313-1450

**DECLARATION UNDER 37 C.F.R. § 1.131**

Sir:

We, Daniel E. Matejczyk and Thomas J. Van Daam, hereby declare and state that:

1. We are inventors of the claimed invention of the above-identified U.S. Patent Application Serial No. 10/263,135.
2. At least as early as December 31, 2001, we reduced to practice our invention as described and claimed in the subject application, generally directed to a method of preparing cryomilled aluminum alloys and components extruded and forged therefrom.
3. Exhibit A (attached) is a copy of the "Nanophase Processing Yield/Scrap Tally" spreadsheet maintained by Raul Perez, working under the supervision of Dan Matejczyk. The spreadsheet shows that alloys were cryomilled as batch numbers NPCxx-05 and NPCxx-06 (portions of batch numbers have been redacted) at least as early as December 31, 2001. Cryomilling is a nanostructured material synthesis technique. Exhibit B (attached) shows handwritten lab notes, dated at least as early as December 31, 2001.

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which indicate the composition of the inert-gas-atomized starting powders that were weighed out and then cryomilled in an attritor. The composition of the metal powder, as indicated, was approximately 8 wt% Mg with the balance of the composition being approximately 92 wt% Al. 8 wt% Mg is well within the 1 atomic% to 11 atomic% range recited in the pending claims of the 10/263,135 application. As indicated on Exhibit A, both samples NPCxx-05 and NPCxx-06 were degassed in Impeller can #3, also designated as "Imp 3". Exhibit C (attached) is a copy of lab notebook pages that evidence the degassing and consolidation procedure applied to the contents of Impeller can #3. Exhibit D (attached) is a copy of hand-written notes showing the extrusion of the resulting consolidated billet from Impeller can #3 at least as early as December 31, 2001. Exhibit E (attached) is a printout of laboratory results, dated at least as early as December 31, 2001, showing the Mg and Fe content of the extruded sample (Imp 3). Finally, Exhibit F (attached) is a copy of test results, dated at least as early as December 31, 2001, showing that the nitrogen content of the extruded sample (Imp 3) is above 0.3 wt%. The resultant nitrogen content indicated at least a 0.3 wt% increase in nitrogen content compared to the alloy powder prior to cryomilling. Dates, personal information, and other information not relevant to the substantiation of invention have been redacted from the copies included in the Exhibits. Although the dates have been redacted, each of Exhibits C, D, E, and F is dated at least as early as December 31, 2001.

4. During production of the Imp 3 sample described above, refractory material was not added to the alloy by anyone associated with production of the alloy. It would have been customary and regular practice to record any additions of refractory materials to the alloy in the cryomilling logs. The lack of any indication, in the cryomilling logs, that refractory material was added is positive evidence that no refractory material was added to the Imp 3 sample.

5. The attached exhibits evidence that, at least as early as December 31, 2001, we reduced to practice a cryomilled aluminum alloy by the steps of: providing a metal

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powder comprising 89 atomic% to 99 atomic% aluminum, 1 atomic% to 11 atomic% of a secondary metal selected from the group consisting of magnesium, lithium, silicon, titanium, zirconium, and combinations thereof; and processing the metal powder with a nanostructured material synthesis technique such that at least 0.3 weight% nitrogen was added to the metal; wherein refractory material was not added to the metal during processing. The exhibits further illustrate that we cryomilled such a powder, removed gaseous components from the cryomilled powder, consolidated the cryomilled powder into a metallic billet, and extruded the metallic billet, at least as early as December 31, 2001.

6. We hereby declare that all statements made herein of our own knowledge are true, and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application of any patent issued thereon.

Daniel E. Matejczyk 10/27/04  
Daniel E. Matejczyk

Thomas J. Van Daam 10/27/04  
Thomas J. Van Daam

CLT01/4675634v3

## Nanophase Processing Yield/Scrap Tally

Run No.	Date	Yield (Kg)	Yield %	Scrap (Kg)	Pwdr in Attrit	Attrit Run'g Tot	Comments

Example 5

REDACTED

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NPC	05	19.625	98%	2.650	-2.275	12.590	R.H 2%.
NPC	06	15.660	78%	3.010	+1.330	13.920	R.H. 4%. Packed impeller can #3 with 6/2 & 6/4 run.

REDACTED

NPC - 05

## Powder Measure

5000g  
5000g  
5000g  
2000g  
-----  
17000g

} C.P. Al  
Batch  
#9 - 8035

in hopper  
825 pm hopper on  
832 LN<sub>2</sub> Thru hopper  
900 powder drop  
950 100 rpm  
510 pm powder dum  
520 in glove box

3000g } 50/50 Al-Mg  
Batch #9 - 7024S

40g Stearic Acid

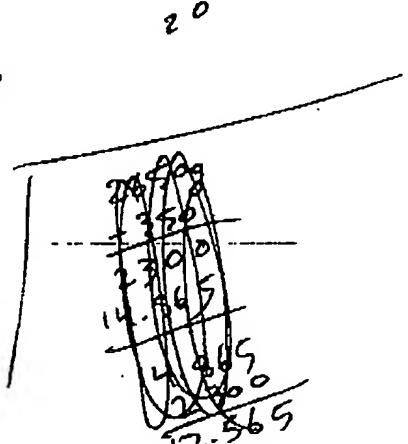
R.H.  $\phi \rightarrow 2\%$

yield  
3705g  
4265g  
4205g  
4845g  
2605g  
-----  
19625

scrap  
2650g

19625  
2650  
-----  
22275

2000



NPC - 06

Powder Measure

5005 g  
 5105 g } C.P. Al  
 4890 g Batch  
 2000 g # 9 - 8035  
17000g

2000 g 50/50 Mg-Al  
 Batch # 9 - 70245

40g Stearic Acid

7<sup>35</sup> in hopper  
7<sup>45</sup> hopper on  
7<sup>51</sup> LN<sub>2</sub> thru hopp  
8<sup>07</sup> powder drop  
8<sup>14</sup> @ 100 rpm  
4<sup>14</sup> powder dump  
4<sup>23</sup> in glove box

yield  
 4250 g  
 4310 g  
 4380 g  
2720g  
15660g

scrap R.H. 4%  
3010g

42 TITLE Degas of Impeller can #3 PROJECT NO. Nanophase A1  
BOOK NO.

Work continued from Page

The powder was brought into the large glovebox and  
5 The can was packed on Can  
welded shut on 33.785 kg.

8:20 AM Can was connected to Vacuum pump.

10:08:30

	Time	Vac	I	Pwr	rpm	Tpump	Ts1	Ts2	Furnace temp set	High Watt
8:33		$4 \times 10^{-2}$ (versus bg)	2.4	116W	38k	26°C				
8:45		$2.05 \times 10^{-4}$	1.7	69W	38k	39°C				
8:53		$9.87 \times 10^{-5}$	1.5	51W	38k	40°C				
9:00		$6.85 \times 10^{-5}$	1.3	43W	38k	40°C	(Chiller switched on)			
9:40		$1.51 \times 10^{-5}$	1.1	32W	38k	34°C				
8:50		$2.88 \times 10^{-5}$	1.0	30W	38k	33°C				

- 25  
9:20 • Vacuum level ~  $3.00 \times 10^{-5}$   $\Rightarrow$  There's a leak.  
• Did a helium leak check, couldn't find a leak.  
30 • Moving the "O" ring results in slight vacuum changes.  $\Rightarrow$  Possible leak  
• Did a 5 min nitrogen purge before exchanging ring  
for a new one.

- 35 • oper to high variance after changing "O" ring, and position  
of "O" ring

SCIENTIFIC BINDERY PRODUCTION CHICAGO 60605 MADE IN USA

Work continued to Page 43

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**TITLE** Degas of Impeller Can #3    **PROJECT NO.** Nanophase Al 43  
**BOOK NO.**

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Time	vac	I	Pwr	rpm	Tpump
10:00	$3.73 \times 10^{-2}$ (Roughing)	24	111	38K	43°C
10:15	$1.23 \times 10^{-2}$ (degassing)	20	84	38K	43°C
10:30	$5.00 \times 10^{-4}$	1.7	64	38K	42°C
10:45	$2.69 \times 10^{-4}$	1.4	50	38K	40°C
11:00	$1.89 \times 10^{-4}$	1.2	45	38K	39°C
11:15	$1.41 \times 10^{-4}$	1.3	41	38K	38°C
11:25	Helium check	70+	140Ks		
11:30	$1.07 \times 10^{-4}$	1.2	38K	38K	37°C
11:35	$9.68 \times 10^{-5}$	1.2	37	38K	37°C
11:45	$8.16 \times 10^{-5}$	1.2	36	38K	37°C
11:50	$7.79 \times 10^{-5}$	1.1	35	38K	37°C
	- completed helium check @ 11:40, no leaks detected				
	- Vacuum is pumping too slow. N2 back purge again (5 min)				
	and moved "O" again. Plus replaced "O" ring.				
	open to high vacuum once again				
	$1.62 \times 10^{-2}$ (Roughing)	2.1	92	38K	46°C
	$7.82 \times 10^{-4}$	2.0	81	38K	45°C
				a/ Roughing Pump	$1.00 \times 10^{-2}$
				Work continued to Page	44

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44 TITLE Degas of impeller can #3 PROJECT NO. Nanophase A1  
BOOK NO.

Work continued from Page 43						
	Time	Vac	I	Pwr	rem	Timp
5	13:00	4.78x10 <sup>-4</sup>	1.7	63W	38K	43°C
10	13:15	2.86x10 <sup>-4</sup>	1.5	53W	38K	42°C
15	13:30	1.78x10 <sup>-4</sup>	1.4	46W	38K	40°C
20	13:45	1.30x10 <sup>-4</sup>	1.3	41W	38K	40°C
25	14:00	9.98x10 <sup>-5</sup>	1.2	37W	38K	39°C
30	14:15	7.76x10 <sup>-5</sup>	1.1	36W	38K	38°C
35	14:30	6.33x10 <sup>-5</sup>	1.1	33W	38K	38°C
40	14:45	5.41x10 <sup>-5</sup>	1.1	32W	38K	37°C
45	15:00	4.91x10 <sup>-5</sup>	1.0	31W	38K	36°C
50	15:15	4.55x10 <sup>-5</sup>	1.0	31W	38K	36°C
55	15:30	4.35x10 <sup>-5</sup>	1.0	30W	38K	36°C
60	15:45	4.17x10 <sup>-5</sup>	1.0	30W	38K	35°C
65	16:00	3.97x10 <sup>-5</sup>	1.0	29W	38K	35°C
70	16:15	3.57x10 <sup>-5</sup>	1.0	29W	38K	35°C
75	16:30	3.75x10 <sup>-5</sup>	1.0	29W	38K	35°C
80	N2 Back Purge (5 min)					
	SCIENTIFIC BINDERY PRODUCTION CHICAGO 60605 MADE IN USA					
	SIGNATURE <i>Laird Piers</i>					

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TITLE Degas of impeller can #3

PROJECT NO. Nanophase A1  
BOOK NO.

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Work continued from Page 44

Time	Vac	I	Pwr	rpm	Tambi
5:16:25	$1.89 \times 10^{-3}$ (Roughing)	5.4	346W	38K	42°C
17:00	$2.00 \times 10^{-2}$ (Roughing)	2.2	96W	38K	45°C
17:15	$4.55 \times 10^{-4}$	1.7	62W	38K	43°C
	Follow up check entire system for leaks				
7:20	$3.85 \times 10^{-5}$	1.0	30W	38K	33°C
	<ul style="list-style-type: none"> <li>• N<sub>2</sub> back purge</li> <li>• changed and moved 'O' ring again.</li> </ul>				
8:05	evacuation tube connected to high vacuum.				
8:30	$2.90 \times 10^{-5}$ (Roughing)	2.3	107W	38K	44°C
8:45	$6.78 \times 10^{-3}$ (Roughing)	1.9	75W	38K	43°C
9:00	$3.59 \times 10^{-2}$	1.5	52W	38K	40°C
9:45	$1.13 \times 10^{-4}$	1.2	39W	38K	38°C
10:15	$7.16 \times 10^{-5}$	1.2	34W	38K	37°C
10:30	$3.74 \times 10^{-5}$	1.1	32W	38K	42°C
	Disconnected chiller				
	Work continued to Page 46				

*R and R*

46 TITLE Degassing of impeller each #3

PROJECT NO. Nanophase A1

BOOK NO.

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Time	Vac	I	Air	rpm	T <sub>pump</sub>
15:35	$3.73 \times 10^{-5}$	1.1	32W	38K	44°C

~~Test Helium leak detector can find leak but not detector~~  
~~Detector not leaky~~

Try to get helium detector to work. Not possible.

14:30	$3.93 \times 10^{-5}$	1.0	30W	38K	43°C
-------	-----------------------	-----	-----	-----	------

No improvement in vacuum reading  $\Rightarrow$  Definite leak

15 Misspec leak detector used to find a small leak in side weld. The side weld was re-welded in 2 spots

15:46 Evacuation began

13:46	$2.59 \times 10^{-4}$	1.8	70W	38K	43°C
-------	-----------------------	-----	-----	-----	------

14:00	$6.79 \times 10^{-5}$	1.2	40W	38K	39°C
-------	-----------------------	-----	-----	-----	------

14:45	$6.23 \times 10^{-5}$	1.0	29W	38K	34°C
-------	-----------------------	-----	-----	-----	------

18:35	$1.00 \times 10^{-6}$	1.0	28W	38K	34°C
-------	-----------------------	-----	-----	-----	------

Good vacuum reading  $\Rightarrow$  no more leaks

9:40	$6.09 \times 10^{-7}$	1.1	30W	38K	33°C
------	-----------------------	-----	-----	-----	------

10:40	$6.05 \times 10^{-7}$	1.1	30W	38K	33°C
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N<sub>2</sub> (as per gr (5 min))

Work continued to Page 47

SCIENTIFIC BINDERY PRODUCTIONS CHICAGO 60605 MADE IN USA

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DATE

**TITLE** Degas of impeller can #3

**PROJECT NO.** Nanophase A1  
**BOOK NO.**

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Work continued from Page 46

Time	Uvac	I	Pwrt	rpm	Tamb	Tc1	Tc2	Furnace temp/sett	High Lvl/1+
11:30	$1.70 \times 10^{-4}$	1.4A	49W	38K	40°C				
13:00	$7.00 \times 10^{-6}$	1.1A	33W	38K	35°C				
14:00	$1.71 \times 10^{-6}$	1.0K	29W	38K	35°C				
14:30	$1.15 \times 10^{-6}$	1.0	29W	38K	35°C				
	$N_2$ Gas back purge (5 min)								
15:45	$1.52 \times 10^{-4}$	1.4	49W	38K	42°C				
17:05	$1.10 \times 10^{-5}$	1.0	29W	38K	37°C				

HOT EVACUATION STARTED / 3 DAY RAMP TO 600°F

8:50	$3.97 \times 10^{-7}$	1.0	26W	38K	35°C	80	80	150/20	
9:55									
9:10	$4.33 \times 10^{-7}$	1.0	27W	38K	35°C	118.2	118.8	150 bold/5min	163
9:25	$5.45 \times 10^{-7}$	1.0	27W	38K	35°C	120.4	118.6	158/25 (30m)	147
9:55	$7.59 \times 10^{-7}$	1.0	27	38	35	138.4	135.8	216/200 bold	206
10:10	$9.41 \times 10^{-7}$	1.0	27	38	36	146.6	143.0	214/30m ramp <sup>200</sup>	205
10:40	$1.70 \times 10^{-6}$	1.0	27	38	36°C	185.0	179.2	300/bold	290
11:40	$7.48 \times 10^{-6}$	1.0	27	38	37°C	300	291	300/350 bold	291
12:10								350 to 160m	

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48 TITLE Degas of impeller can #3

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	Time	Vac	I	Pwr	rpm	T <sub>ump</sub>	T <sub>SJ</sub>	T <sub>C2</sub>	Temp	High Volt
5	12:38	$1.77 \times 10^{-5}$	1.0A	27W	38K	37°C	268.6	258.6	258.6	341
10	13:10	$2.59 \times 10^{-5}$	1.0A	28W	38K	38°C	277.6	273.0	375 ramp to 375 hold	342
15	13:40	$2.98 \times 10^{-5}$	1.0A	28W	38K	38°C	293.6	289.4	375 hold 30m	367
20	14:25								ramp to 400 hold	376
25	14:52	$3.24 \times 10^{-5}$	1.0A	28W	38K	38°C	301.8	306.2	306.2	376
30	14:55	$3.15 \times 10^{-5}$	1.0A	28W	38K	38°C	321.8	318.4	400 hold	394
35	16:00	$2.86 \times 10^{-5}$	1.0A	28W	38K	37°C	337.8	344.8	400 hold	395
40	17:00	$2.46 \times 10^{-5}$	1.0A	28W	38K	36°C	346.2	343.8	400 hold	395
45	8:20	$8.69 \times 10^{-6}$	1.0	28W	38K	33°C	384.2	382.8	400 hold	399
50	8:30	$8.71 \times 10^{-6}$	1.0	28W	38K	33°C	384.2	383.0	450/30	399
55	8:45	$8.90 \times 10^{-6}$	1.0	29W	38K	32°C	385.8	384.6	450/30	445
60	9:00	$8.91 \times 10^{-6}$	1.0	29W	38K	32°C	390.6	389.0	450 hold	444
65	9:15	$9.46 \times 10^{-6}$	LG	29W	38K	32°C	399.4	392.6	450/hold	448
70	9:30	$1.0 \times 10^{-5}$	1.0	29W	38K	32°C	397.0	395.0	500/30	448
75	9:45	$1.0 \times 10^{-5}$	1.0	29W	38K	32°C	405.2	403.2	500/30	475

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Work continued to Page 49

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TITLE Impeller can #3

PROJECT NO.  
BOOK NO.

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Work continued from Page 48

Time	Vol	I	Pwr	rev	T <sub>avg</sub>	Tc.	Tch	Furnace temp/set	High limit
10:00	1.82x10 <sup>-5</sup>	1.0	29W	38K	32°C	415.2	413.2	500/hold	497
10:15	1.42x10 <sup>-5</sup>	1.0	29W	38K	31°C	421.4	419.4	500/hold	495
10:30	1.69x10 <sup>-5</sup>	1.0	29W	38K	31°C	426.2	424.2	525/30	495
10:45	1.98x10 <sup>-5</sup>	1.0	29W	38K	31°C	432.4	430.2	525/30	508
11:00	2.42x10 <sup>-5</sup>	1.0	29W	38K	31°C	441.8	439.6	525/hold	521
11:15	2.78x10 <sup>-5</sup>	1.1	29W	38K	31°C	449.4	448.6	525/hold	519
11:30	3.19x10 <sup>-5</sup>	1.1	29W	38K	31°C	449.4	447.4	525/hold	520
11:45	3.63x10 <sup>-5</sup>	1.1	29W	38K	31°C	453.2	451.4	525/hold	525
12:00	4.21x10 <sup>-5</sup>	1.1	30W	38K	31°C	463.8	462.0	525/hold	565
12:15	4.69x10 <sup>-5</sup>	1.1	30W	38K	31°C	467.0	465.4	525/hold	565
12:30	5.69x10 <sup>-5</sup>	1.1	30W	38K	31°C	470.6	469.0	550/30	563
12:45	6.28x10 <sup>-5</sup>	1.1	31W	38K	31°C	476.6	475.2	550/30	580
13:00	7.23x10 <sup>-5</sup>	1.1	31W	38K	30°C	484.4	483.4	550/hold	596
13:15	8.73x10 <sup>-5</sup>	1.1	31W	38K	30°C	490.0	488.6	550/hold	565
13:30	9.88x10 <sup>-5</sup>	1.1	32W	38K	30°C	493.6	492.2	550/hold	564
13:45	1.19x10 <sup>-4</sup>	1.2	33W	38K	31°C	496.8	495.4	550/hold	563

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50 TITLE impeller can #3

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							Furnace	High		
	Time	Vac	I	Pwr	R.P.M	T <sub>pump</sub>	T <sub>c1</sub>	T <sub>c2</sub>	tempset	limit
5	14:00	1.44 $\times 10^{-4}$	1.2	33 W	38 K	31°C	499.2	497.8	550/hold	563
14:15		1.74 $\times 10^{-4}$	1.2	34 W	38 K	31°C	506.2	500.0	550/hold	563
14:30		2.07 $\times 10^{-4}$	1.3	35 W	38 K	31°C	503.0	501.8	550/hold	563
10		Roughing Pump		1.97 $\times 10^{-3}$						
14:45		2.48 $\times 10^{-4}$	1.3	36 W	38 K	31°C	505.0	503.4	550/hold	562
15:00		2.91 $\times 10^{-4}$	1.3	39 W	38 K	32°C	506.2	504.8	550/hold	562
15		Roughing Pump		7.53 $\times 10^{-3}$						
15:15		3.36 $\times 10^{-4}$	1.4	41 W	38 K	32°C	507.4	506.2	550/hold	562
		Roughing Pump		1.3 $\times 10^{-2}$						
15:30		5.03 $\times 10^{-4}$	1.5	45 W	38 K	32°C	508.8	507.6	550/hold	562
15:45		2.20 $\times 10^{-4}$	1.7	54 W	38 K	33°C	510.2	508.8	550/hold	561
16:00		Roughing Pump		4.72 $\times 10^{-2}$						
16:15		3.04 $\times 10^{-4}$	1.8	62 W	38 K	33°C	510.8	509.6	550/hold	561
		Roughing Pump		7.44 $\times 10^{-2}$						
16:30		4.46 $\times 10^{-4}$	2.0	73 W	38 K	34°C	511.8	510.2	550/hold	561
		Roughing Pump		1.23 $\times 10^{-1}$						
16:45		6.29 $\times 10^{-4}$	2.2	85 W	38 K	35°C	512.6	511.2	550/hold	561
		Roughing Pump		1.84 $\times 10^{-1}$						
17:00		8.30 $\times 10^{-4}$	2.4	99 W	38 K	36°C	513.4	511.8	550/hold	561
		Roughing Pump		2.47 $\times 10^{-1}$						
17:15		2.5	109 W	38 K	37°C	514.0	512.6			560
		Roughing Pump		3.05 $\times 10^{-1}$						
17:30		2.6	115 W	38 K	38°C	514.8	513.2	550/hold		560
		Roughing Pump		3.54 $\times 10^{-1}$						
17:45		2.7	121 W	38 K	39°C	515.4	513.8			561
		Roughing Pump		3.95 $\times 10^{-1}$						

SOUTHERN ENDERBY PRODUCTIONS CHICAGO 60608 MADE IN USA

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DATE

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WITNESS

TITLE impeller can #3

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Work continued from Page 50

			I	Pwr	rpm	Tamp:	Tc1	Tc2	Furnace temp/rot	High limit
5	17:45		2.7	122W	38K	39°C	516.0	514.4	550/hold	560
						Roughing Pump $3.96 \times 10^{-1}$				
10	18:00		2.7	120W	38K	40°C	516.6	515.0	550/hold	560
						Roughing Pump $3.84 \times 10^{-1}$				
15	18:15		2.6	119W	38K	40°C	517.0	515.4	550/hold	560
						Roughing Pump $3.57 \times 10^{-1}$				
20	18:30		2.5	112W	38K	40°C	517.4	515.8	550/hold	560
						Roughing Pump $3.12 \times 10^{-1}$				
25	18:45		2.3	105W	38K	40°C	517.8	516.2	550/hold	560
						Roughing Pump $2.65 \times 10^{-1}$				
30	8:45	$7.59 \times 10^{-5}$	1.1	33W	38K	33°C	522.2	520.8	575/30	559
	9:00	$7.52 \times 10^{-5}$	1.1	32W	38K	33°C	525.6	524.4	575/30	575
	9:15	$7.70 \times 10^{-5}$	1.1	32W	38K	33°C	529.8	529.4	575/hold	589
	9:45	$8.27 \times 10^{-5}$	1.1	32W	38K	34°C	535.6	534.4	575/hold	587
	10:19	$8.83 \times 10^{-5}$	1.1	33W	38K	34°C	538.4	537.2	575/hold	587

Work continued to Page 52

SCIENTIFIC BINDERY PRODUCTION CHICAGO 60605 MADE IN USA

DATE

DATE

52 TITLE impeller can #3

PROJECT NO.

BOOK NO.

Work continued from Page 51

	VAC	I	Pwr	rpm	T <sub>avg</sub>	T <sub>C1</sub>	T <sub>C2</sub>	Burnout Temp Set	High Limit
5	10:45 $7.99 \times 10^{-5}$	1.1	33W	38k	35°C	539.6	541	610/30	587
10	11:15 $9.90 \times 10^{-5}$	1.1	33W	38k	35°C	554.4	553.4	610/bad	630
15	13:00 $1.52 \times 10^{-4}$ roughing pump $6.86 \times 10^{-3}$	1.2	37	38k	37°C	567.6	568.4	610/bad	623
20	14:15 $1.64 \times 10^{-4}$ roughing pump $8.14 \times 10^{-3}$	1.3	37	38k	38°C	573.6	572.4	625/30	621
25	15:10 $1.70 \times 10^{-4}$ roughing pump $9.22 \times 10^{-3}$	1.3	38	38k	38°C	583.4	582.2	625/Local	638
30	16:00 $1.72 \times 10^{-4}$	1.3	38	38k	38°C	557.2	586.0	625/Local	637
35	17:00 $1.59 \times 10^{-4}$ roughing pump $7.50 \times 10^{-3}$	1.3	38	38k	38°C	587.8	588.8	625/Local	636
40	09:00 $2.49 \times 10^{-5}$	1.0	28W	38k	35°C	594.0	592.4	625/Local	635
45	09:10 $2.52 \times 10^{-5}$	1.0	28W	38k	35°C	594.0	592.6	632/Local	635
50	09:30 $2.55 \times 10^{-5}$	1.0	28W	38k	35°C	596.8	595.2	632/Local	643
55	10:30 $2.57 \times 10^{-5}$	1.0	28	38k	34°C	598.6	597.2	632/Local	643
60	12:00 $2.47 \times 10^{-5}$	1.0	28	38	34°C	599.6	598.2	632/Local	642
65	13:00 $2.20 \times 10^{-5}$	1.0	27	38	37°C	600.6	599.2	632/Local	642
70	17:38 $1.93 \times 10^{-5}$	1.0	28W	38k	36°C	600.8	599.6	632/Local	642

SCHERFFER BINDERY PRODUCTIONS CHICAGO 00005 MADE IN USA

Work continued to Page 53

2 min 2 - 9 min 2

DATE

RECEIVED AND UNDERSTOOD BY

DATE

WITNESS

DATE

53

TITLE Impeller Can #3

PROJECT I.W.  
BOOK NO.

Work continued from Page 52

Time	N.c.	I	Pwr	rem	Timp	Tc	Tc2	Furnace temp/set	Stab limit
09:30	$9.60 \times 10^{-6}$	1.0	27 W	38 K	34°C	600.4	599.0	632/600/1	642
10:30	$2.85 \times 10^{-6}$	1.0	28 W	38 K	32°C	600.0	598.6	632/600	641
10:41	$2.85 \times 10^{-6}$	1.0	26 W	38 K	32°C	600.2	598.8	632/600	641
• Shaft furnace off and chamber									
10:40	$1.33 \times 10^{-6}$	1.0	27 W	38 K	33°C	470.6	475.6		
10:40	$7.73 \times 10^{-7}$	1.0	26 W	38 K	34°C	444.4	445.8		
10:40	$2.81 \times 10^{-7}$	0.9	26 W	38 K	34°C	400.6	402.2		
10:43	$1.45 \times 10^{-7}$	0.9	26 W	38 K	35°C	372.6	374.6		
10:43	$6.05 \times 10^{-8}$	0.9	25 W	38 K	35°C	311.6	312.2		
10:40	$5.36 \times 10^{-8}$	0.9	25 W	38 K	35°C	275.2	250.6		
• Thermal couples disconnected.									
• Tube ruptured.									
(Ultimate Iacqua, $2.56 \times 10^{-9}$ + 40 minutes)									
10:45	$5.12 \times 10^{-8}$	0.9	25 W	38 K	35°C				
• Tube welded									
• Vacuum level jumped all around and peaked (0) $7.01 \times 10^{-8}$									
10:48	$5.12 \times 10^{-8}$								
Work continued to Page 54									

© BURGESS PRODUCTIONS CHICAGO 60605 MADE IN USA

P-Tech and Perley

DATE

WITNESS

DATE

DATE

54 TITLE Impeller can #3

PROJECT NO. Nanophase A1  
BOOK NO.

Work continued from Page 53

Final Mass of can 33.665 Kg  
 Tube cut off 0.045 Kg  
~~33.710~~

Initial can mass 33.745 Kg

• Tube was cut 3 times.

Can was shipped out on

10/28

SCIENTIFIC SINDERY PRODUCTIONS CHICAGO 60603 MADE IN USA

Work continued to Page

DATE

DATE

DATE

SIGNATURE

Doris Z. Gammie

RECORDED TO AND UNDERSTOOD BY

DATE

WITNESS

IMP1

4 INDUCERS (9,14,17)(12)

IMP2SHIPPED IMP3 & IMP4 ON AUG 20 (MID SEPT. EXTRUSION)  
\* FINAL FORNACE SETPOINT WAS 371°F

IMP2 LOADED INTO FURNACE @ 8100am.

TIME BILLET TEMP FURNACE TEMP  
T/C #2 T/C #331/12 PREHEAT BILLET LOADED @ 10:30 AM  
1:30 PM + 0.25%

8°F

REFDAC TE D

BEST AVAILABLE COPY

BREAK THROUHT F<sub>TONS</sub> = 4237 TONS

IMP 3 &amp; 4

	BILLET TEMPS	FURNACE	
1:00am.	#2	#3	
	T/C 2	T/C #3	FURNACE SETPOINT DROPPED
	4		FROM 410 → 400
7:15am	FURNACE 389.2	400.5	BILLET 4
	7 (BILLET 3)		9-30-98 - IMP 4 [TOOK JACKET]
	388.2		
7:30am.	389.1	400.3	
7:40am	389.3	400.8	... FROM 400 → 376°F
8:45am	389.3	391.6	
	380.8	386.2	386.2 ... FROM 376 → 369°F
9:05am.	377.1	382.3	... 8:58 369 → 364
9:30am	372.2	378.5	381.0
	371	378.0	376.5 364 → 368
9:46	370.	375.	375.
			LINER 634°F
			377 (DIE 200 → NEAR TO 400°F) @ 9:30
PULSED FIRST.			
960 PULST HRSN			

PULSED LOAD 3:45AM @ 400°F  
200°F @ 4:10 AM  
350°F @ 6:00AM  
380°F @ 7:00AM

10:30

**THE BOEING COMPANY**  
**Rocketdyne Propulsion**  
**And Power System**  
**MATERIALS APPLICATION**  
**PROCESS**  
**LABORATORY OPERATIONS**

<u>DATE</u>	<u>G.O.</u>	<u>REFERENCE</u>	<u>REPORT No.</u>
	61918	EWR#936081	9811-4
<u>PROGRAM NAME</u>		<u>QUANTITY</u>	
Nanophase Aluminum		2	
<u>MATERIAL</u>		<u>SPECIFICATION</u>	
Aluminum Alloy			
<u>SUBMITTED BY</u>		<u>DEPT.</u>	<u>PHONE</u>
R. Perez		912	3958
		LOCATION	
		CANOGA	

**TEST REPORT****LABORATORY TEST RESULTS****BEST AVAILABLE COPY**

<u>SAMPLE</u>	<u>Mg %/wt</u>	<u>Iron %/wt</u>
9/30 IMP3	8.8	0.1
9/30 IMP4	8.6	0.1

Log No. 9811-4  
 Charge No. 24410-61918-98100  
 Notebook Page No. 2054-24

W. Ho  
 ANALYST

DATE

A. Apari (W. Ho)  
 APPROVED

DATE



**LECO CORPORATION**  
**3000 Lakeview Avenue**  
**St. Joseph, Michigan 49085-2386**

Work Order No: 12636  
Classification: S  
PO/WO No: NR98439823  
Customer No: 2593  
Account No: 109495

## CUSTOMER SERVICE ANALYSIS REPORT

Customer: BOEING NORTH AMERICAN, INC.  
ROCKETDYNE DIVISION/833 CANOGA AVE.  
CANOGA PARK CA 91303

Attention: SONYA REID Dept. 817, MC BA71

The following is our laboratory analysis report on samples submitted by your company.

Any additional details of this analysis report can be obtained from the Technical Services Laboratory.  
Call 616-982-2277.

*NOTE: We request that all samples submitted to the LECO® Technical Services Laboratory be accompanied by a Material Safety Data Sheet (MSDS) describing each material's characteristics. This information permits proper handling and storage.*

Results for Sample: 63681	IMP3	Al7.5%Mg
---------------------------	------	----------

Instrument: CS444

Standard: NIST 125b @ 0.028% C

Remarks: Preheated Crucible 528-018, Preheated Lid 528-043, ~1 g Lecocel II HP 502-173, ~1 g Iron Chip 502-231

Preparation: Abraded with a file, sectioned with a shear, rinsed in acetone and dried with warm air.

% Sulfur	% Carbon
0.152	
0.151	
0.148	

Instrument: RH402

Standard: Hydrogen Gas Dose

Remarks: 769-781 Crucible

Preparation: Abraded with a file, sectioned with a shear, rinsed in acetone and dried with warm air.

Hydrogen ppm	Bulk ppm	Surface ppm
43.09	42.78	0.311

Instrument: TC438

Standard: LECO Std. 501-044 @ 0.0107% O, 0.0071% N (J0215-2)

Remarks: 782-720 Crucible, 1 g Nickel Basket 502-344, 0.05 g Graphite Powder 501-073

Preparation: Abraded with a file, sectioned with a shear, rinsed in acetone and dried with warm air.

% Nitrogen	% Oxygen
0.383	0.239
0.381	0.235